10/524366

(19) World Intellectual Property Organization

International Bureau

11 March 2004 (11.03.2004)





PCT

(10) International Publication Number WO 2004/020531 A1

(51) International Patent Classification⁷: C09D 7/12

C09C 1/30,

(21) International Application Number:

PCT/EP2003/008329

(22) International Filing Date:

29 July 2003 (29.07.2003)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data: 102 39 424.5

28 August 2002 (28.08.2002) DE

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- (81) Designated States (national): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU,

CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.

(84) Designated States (regional): European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, RO, SE, SI, SK, TR).

Declarations under Rule 4.17:

- as to applicant's entitlement to apply for and be granted a patent (Rule 4.17(ii)) for the following designations AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG. KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, UZ, VC, VN, YU, ZA, ZM, ZW, European patent (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PT, RO, SE, SI, SK, TR)
- of inventorship (Rule 4.17(iv)) for US only

Published:

with international search report

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: SILICAS

(57) Abstract: Silanised, structurally modified silicas, characterised by groups fixed on the surface, the groups being alkylsilyl (SiC_nH_{2n+1}, with n=2 - 18). They are produced in that pyrogenically produced silicas are treated with the silanising agent and structurally modified. They are used to improve scratch resistance in lacquers.



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Silicas

The invention relates to silanised, structurally modified, pyrogenically produced silicas, a process for the production thereof and their use.

5 Silanised silicas are used as thickeners, such as e.g. for water-thinnable lacquers and resins, such as e.g. epoxy resins.

From EP 0 672 731 B1, silanised, pyrogenically produced silicas are known, which are characterised in that the pyrogenically produced silicas are treated with a compound from the group (RO)₃SiC_nH_{2n+1}, wherein n=10 to 18 and R= short-chained alkyl radicals. For example, the pyrogenically produced silicas have been treated with the compound (CH₃O)₃SiC₁₆H₃₃ (hexadecyltrimethoxysilane) or with the compound (CH₃O)₃SiC₁₆H₃₇ (octadecyltrimethoxysilane).

The production of the silanised, pyrogenically produced silicas takes place in that the pyrogenically produced silicas are placed in a mixer, the silicas are sprayed, optionally first with water and then with the compound from the group $(RO)_3SiC_nH_{2n+1}$ while mixing intensively, mixed for a further 15 to 30 minutes and then tempered at a temperature of 100 to 160°C for a period of 1 to 3 hours.

The invention provides silanised, structurally modified, pyrogenically produced silicas characterised by groups fixed on the surface, the groups being alkylsilyl (SiC_nH_{2n+1}, with n=2 - 18), preferably octylsilyl and/or hexadecylsilyl.

The silica according to the invention can have the following physico-chemical characteristics:

BET-surface area m2/g: 25 - 400

Average size of the

primary particles nm: 5 - 50

pH value: 3 - 10

5 Carbon content %: 0.1 - 25

DBP value %: The DBP value is at least 10%

lower than the DBP value of the

corresponding silanised, non-

structurally modified silica. With

10 very marked structural

modification, the structure can be broken down in such a way that the

DBP value can no longer be

determined.

15 A silica produced by a high-temperature hydrolysis route from $SiCl_4 + H_2$ and O_2 can be used as the pyrogenically produced silica.

In particular, a silica produced by high temperature hydrolysis having the following physico-chemical

20 characteristics can be used:

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	AEROSIL 90	AEROSIL 130	AEROSIL 150	AEROSIL 200	AEROSIL 300	AEROSIL 380	AEROSIL OX 50	AEROSIL TT 600
Behaviour in respect of water				hydro	hydrophilic			
Appearance				loose whi	loose white powder			
BET surface area 1) m^2/g	90 ± 15	130 ± 25	150 ± 15	200 ± 25	300 # 30	380 ± 30	50 ± 15	200 ± 50
Average size of the	20	16	14	12	7	4	40	40
mti								
primary particles								
Tamped density 2)						,		
standard material	ca. 80				ca. 50	ca. 50	ca. 130	ca. 60
T/6	1	ca. 120	Ca. 120	Ca. 120	ca. IZO	Ca. 120) 	1
compacted material								
g/1								
(additive "V")								
Loss on drying 3)								!
(2 hours at 1000°C) %	< 1.0	< 1.5	< 0.5 9)	< 1.5	< 1.5	< 1.5	< 1.5	< 2.5
on leaving supplier's works								
Loss on ignition $^4)^7$) &	< 1	< 1	< 1	< 1	v 2	< 2.5	۲۱ ۷	< 2.5
(2 hours at 1000°C)								
pH value ⁵) (in 4%	3.6-4.5	3.6-4.3	3.6-4.3	3.6-4.3	3.6-4.3	3.6-4.3	3.8-4.8	3.6-4.5
aqueous dispersion)								
SiO ₂ 8)	8.66 <	8.66 <	8.66 <	8.66 <	8.66 <	8.66 <	> 99.8	> 99.8
A1 ₂ 0 ₃ 8)	< 0.05	< 0.05	< 0.05	< 0.05	< 0.05	< 0.05	< 0.08	< 0.05
Fe ₂ O ₃ 8)	< 0.003	< 0.003	< 0.003	< 0.003	< 0.003	< 0.003	< 0.01	< 0.003
rio ₂ 8)	< 0.03	< 0.03	< 0.03	< 0.03	< 0.03	£0.0 >	< 0.03	< 0.03
HC1 8) 9) &	< 0.025	< 0.025	< 0.025	< 0.025	< 0.025	< 0.025	< 0.025	< 0.025
Sieving residue 6) &	< 0.05	< 0.05	< 0.05	< 0.05	< 0.05	< 0.05	< 0.2	< 0.05
(acc. to Mocker, 45 μm)								

- 1) based on DIN 66131
- 2) based on DIN ISO 787/XI, JIS K 5101/18 (not sieved)
- 3) based on DIN ISO 787/II, ASTM D 280, JIS K 5101/21
- 4) based on DIN 55 921, ASTM D 1208, JIS K 5101/23
- 5) based on DIN ISO 787/IX, ASTM D 1208, JIS K 5101/24
- 6) based on DIN ISO 787/XVIII, JIS K 5101/20 7) based on the substance dried for 2 hours at 105°C
- 8) based on the substance ignited for 2 hours at $1000^{\circ}\mathrm{C}$
- 9) HCl content is a component of the loss on ignition

Pyrogenic silicas of this type are known. They are described, inter alia, in:

Winnacker-Küchler, Chemische Technologie, volume 3 (1983), 4th edition, page 77 and

5 Ullmanns Encyklopädie der technischen Chemie, 4th edition (1982), volume 21, page 462.

The pyrogenically produced silicas are treated with a compound from the group $(RO)_3SiC_nH_{2n+1}$, wherein n=2 to 18 and R= alkyl, such as e.g. methyl, ethyl or similar.

10 In particular, the following compounds can be used:

Silane I $(CH_3O)_3SiC_{16}H_{33}$ (hexadecyltrimethoxysilane)

Silane II (CH₃O)₃SiC₈H₁₇ (octyltrimethoxysilane)

The silicas according to the invention can be produced in that the pyrogenically produced silicas are placed in a mixer, the silicas are sprayed, optionally first with water and then with the compound (organosilane) from the group (RO)₃SiC_nH_{2n+1} while mixing intensively, mixed for a further 15 to 30 minutes and then tempered at a temperature of 100 to 160°C for a period of 1 to 3 hours, structurally modified and/or optionally post-ground. A further tempering can optionally take place after the structural modification and/or post-grinding.

The structural modification can take place e.g. with a ball mill or a continuously operating ball mill. The post25 grinding can take place e.g. using an air-jet mill or pin mill. The tempering can take place batchwise, e.g. in a drying cupboard, or continuously, e.g. in a fluidised bed. The tempering can take place under protective gas, e.g. nitrogen.

30 The water used can be acidified with an acid, e.g. hydrochloric acid, down to a pH value of 7 to 1.

The organosilane used can be dissolved in a solvent, such as e.g. ethanol.

The tempering can be performed in a protective gas atmosphere, such as e.g. under nitrogen.

5 The pyrogenically produced silicas according to the invention silanised with silane I have the physico-chemical characteristics listed in Table 2 before structural modification:

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Educt	A 90	A 130	A 150	A 200	A 300	A 380	0X 20	TT 600
Average size of the primary particles [nm]	20	16	14	12	7	7	40	40
BET surface area [m²/g]	40 - 90	60 - 130	75 - 150	100 - 200	150 - 300	200 - 380	20 - 50	100 - 250
Tamped density [g/1]	40 - 140	40 - 140	40 - 140	40 - 140	40 - 140	40 - 140	40 - 140	40 - 140
Loss on drying [%]	< 2		< 2	< 2	< 2	< 2	. 2	2
Loss on ignition [%]	0.1 - 10	0.1 - 10	0.1 - 10	0.5 - 15	0.5 - 20	0.5 - 25	0.1 - 10	0.1 - 20
C content [%]	0.1 - 10	0.1 - 10	0.1 - 10	0.5 - 15	0.5 - 20	0.1 - 25	0.1 - 10	0.5 - 20
pH value	3.5 - 5.5	3.5 - 5.5	3.5 - 5.5	3.5 - 5.5	3.5 - 5.5	3.5 - 5.5	3.5 - 5.5	3.5 - 5.5

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The silanised, structurally modified, pyrogenically produced silicas according to the invention can be used to improve scratch resistance in lacquers.

5 Examples

The pyrogenically produced silicas used have the physicochemical characteristics listed in Table 1.

As organosilanes, the following compound with the general formula $(RO)_3SiC_nH_{2n+1}$ is used:

10 (Silane I) $(CH_3O)_3SiC_{16}H_{33}$

The silica is placed in a mixer and sprayed first with water and then with organosilane, mixing intensively.

When the spraying is complete, stirring is continued for a further 15 to 30 minutes and then the mixture is tempered for 1 to 3 hours at 100 to 160°C. The tempering can also take place under protective gas, e.g. nitrogen.

The individual reaction conditions can be taken from Table 3.

20 The physico-chemical characteristics of the silanised silicas obtained are listed in Table 4.

c	n

Tempering temperature (°C)	120	140	140	140	140	140
Tempering period (h)	2	2	2	2	2	7
Ethanol quantity (g/100 g Aerosil)	6	0	0	0	0	0
Water quantity (g/100 g Aerosil)	0	0	5	2.5	1.25	1.25
Silane quantity (g/100 g	Н	2.5	20	10	S	2.5
Silane	Silane I					
Aerosil	A 300	A 200				
Example Aerosil	Н	2	3	4	D.	9

able

Example	pH value	Tamped density (g/1)	C content (%)	Surface area (m²/g)	Loss on drying (%)	Loss on ignition (%)
П	4.3	50	1.3	253	0.4	1.8
2	4.4	49	1.7	176	0.3	2.5
m	4.6	89	10.1	116	9.0	12.7
4	4.5	72	5.7	144	9.0	7.1
2	4.7	52	2.6	167	9.0	3.4
9	4.5	51	1.9	171	0.7	2.5

Production and physico-chemical properties of the silicas according to the invention

Production of the silicas according to the invention:

The silicas, which can be produced as described in EP 0 672 5 731, are then structurally modified by mechanical action and possibly post-ground in a mill. A tempering can possibly take place after the structural modification and/or post-grinding.

The structural modification can take place e.g. with a ball 10 mill or a continuously operating ball mill. The postgrinding can take place e.g. using an air-jet mill or pin mill. The tempering can take place batchwise, e.g. in a drying cupboard, or continuously, e.g. in a fluidised bed. The tempering can take place under protective gas, e.g. 15 nitrogen.

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<u>Table 5</u> Overview of the production of the comparative silicas and the silicas according to the invention (Examples)

Designation	Surface-fixed group	Structural modification	Post-grinding after structural modification	Tempering after post-grinding
Comparative silica 1	Hexadecylsilyl	No		1
Comparative silica 2	Octylsilyl	No	1	ı
Silicas 1	Hexadecylsilyl	Yes	No	No
Silicas 2	Octylsilyl	Yes	Yes	No
Silicas 3	Hexadecylsilyl	Yes	Yes	Yes
Silicas 4	Octylsilyl	Yes	No	Yes
Silicas 5	Octylsilyl	Yes	Yes	No
Silicas 6	Hexadecylsilyl	Yes	Yes	No
Silicas 7	Hexadecylsilyl	Yes	Yes	No
Silicas 8	Hexadecylsilyl	Yes	No	No
Silicas 9	Octylsilyl	Yes	Yes	No
Silicas 10	Octylsilyl	Yes	No	No
Silicas 11	Octylsilyl	Yes	Yes	No
Silicas 12	Octylsilyl .	Yes	No	No

Table 6: Physico-chemical data of the silicas according to the invention (Examples) and the comparative silicas

•							
Designation	Tamped	ross on	ross on	pH value	pH value C content [%] DBP	DBP	BET specific
	density	drying [%]	ignition	ı		adsorption	surface area
	[g/1]		&			[8]	[m²/g]
Comparative silica 1	22	0.5	1.8	4.6	1.2	302	195
Comparative silica 2	51	9.0	8.9	5.3	5.4	263	175
Silicas 1	137	0.7	1.9	4.9	1.3	217	193
Silicas 2	112	0.7	7.0	5.8	5.5	145	175
Silicas 3	118	0.7	2.3	5.1	1.3	228	176
Silicas 4	163	6.0	6.7	5.3	5.4	134	176
Silicas 5	114	0.5	7.1	6.0	5.4	142	175
Silicas 6	113	1.3	2.2	5.1	1.4	221	193
Silicas 7	123	0.7	2.6	0.9	1.4	208	161
Silicas 9	146	1.1	2.3	5.8	1.4	182	195
Silicas 9	240	8.0	6.7	4.8	5.3	87	691
Silicas 10	322	0.3	6.9	0.9	5.3	Could not	172
						pe	
•						determined	
Silicas 11	204	2.0	6.4	5.7	5.4	101	173
Silicas 12	276	0.3	9.9	9.9	5.3	Could not	168
						pe	
						determined	

Application examples

Example 1:

For the investigation of the improvement in scratch resistance, a conventional 2-component polyurethane lacquer was used. The formulation of the lacquer and its production, including application, are summarised below:

Formulation:

	,
Millbase	Parts
	by wt.
Acrylic resin, 50% in xylene/ethylbenzene 3:1	53.3
nergite resim, 500 in Agrene, congressione over	
Butyl acetate 98%	6.7
Xylene	6.7
vAtene	"
Silica	5.0
~	71.7
2	/ /
Lacquer make-up	
Acrylic resin, 50% in xylene/ethylbenzene 3:1	1.1
Xylene	12.2
Ethoxypropyl acetate	1.5
Telloxypropyr decedee	
Butyl glycol acetate	1.5
Butyl acetate 98%	<u> </u>
Bucyl acecate 30%	
Aliphatic polyisocyanate, approx. 75% in 1-	17.0
methoxypropyl-2-acetate/xylene 1:1	
Σ	105.0
	J

Binder concentration: 40%
Silica calculated on the basis of millbase (solids): 18.8%
Silica calculated on the basis of lacquer (total): 5.0%
Silica calculated on the basis of lacquer (solids): 12.5%

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Production and application of lacquers

The binder is mixed with the solvents. Then, for the purpose of predispersion, the silica is incorporated into this mixture with the high-speed mixer (disk \varnothing 45 mm) and 10 predispersed for 5 min at 2000 rpm. The mixture is dispersed in a laboratory pearl mill for 30 min at 2500 rpm and 60% pump capacity using glass beads (\varnothing approx. 1 mm). The millbase is tested with a grindometer, 25 μ m, according to DIN ISO 1524. It must be smaller than 10 μ m.

15 The conversion of the millbase to lacquer takes place in accordance with the formulation, the components being mixed at 2000 rpm with a vane agitator. The hardener is incorporated in the same way.

After adjusting the lacquers to spray viscosity in accordance with DIN 53411, the lacquers are applied to black lacquered metal sheets, e.g. DT 36 (from Q-Panel), by spray application (coat thickness about 40-50 μ m). After spraying, the metal sheets are dried for 24 h at room temperature and then for 2 h in a drying oven at 70°C.

Scratch tests:

The metal sheets are abraded with a quartz/water slurry (100 g water + 1 g Marlon A 350, 0.25% + 5 g Sikron F500) and with a CaCO₃/water mixture (100 g water + 1 g Marlon A 350, 0.25% + 5 g Millicarb BG) using an abrasion and washing resistance tester (Erichsen, brush with hog's bristles). The gloss before and 10 min after the abrading is determined with a reflectometer (20° irradiation angle).

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Table 7: Summary of the properties of the liquid lacquers relevant in terms of lacquer technology, and of the applied and dried films.

	Comparative silica 1	Silica 7	Silica 8	Reference without silica	Comparative silica 2	Silica 9	Silica 11	Reference without silica
Grindometer value [µm]	. < 10	< 10	. 10	< 10	< 10	< 10	< 10	\
Viscosity (millbase) [mPas] 6 Rpm	409	210	220	/	2670	935	832	``
60 Rgm	407	210	212	,	1260	409	407	_
Viscosity (lacquer + hardener) [mPas] 6 rpm	120 113	80	80	60	446 194	195 146	175	55
Flow	poor fine cracks	OK	OK	ОК	Orange peel effect	OK	OK	ОК
Scratch resistance							:	
20° reflectometer value before scratching	81	89.5	89.1	91.3	38	85.5	85.3	91.7
Haze before scratching	101	6	12	2	423	18	19	7
Black value My	272	286	286	291	260	283	282	294
40 strokes with Sikron F 500 residual gloss [%]	83.4	88.5	90.7	51.8	,	80.4	84.3	56.1

The silicas 7 + 8 and 9 + 11 according to the invention can be used in high concentrations without impairing the appearance of the lacquer surface owing to their substantially lower rheological efficiency compared with comparative silica 1 + 2. In addition, the silicas according to the invention display a substantial improvement in scratch resistance of the lacquer surface.

Example 2

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In this example the influence of the structural

modification was investigated on the basis of a high solids
2-component PU clear lacquer. The formulation of the
lacquer and its production, including application and
testing, are summarised below:

Formulation:

Millbase	Parts by wt.
Acrylic copolymer, mod. with synthetic fatty acids, 70% in n-butyl acetate	61.0
Butyl acetate 98%	7.3
Methoxypropyl acetate	1.7
Solvesso 100	2.0
<pre>Xylene Baysilon OL 17, 10% in xylene (silicone oil)</pre>	2.0
Silica	5.0
Σ	79.7
Lacquer make-up (hardener)	
Aliphatic polyisocyanate, 90% in n-butyl acetate	22.3
Butyl acetate 98%	2.0
Solvesso 100	1.0
Σ	105.0

Binder concentration: 62.8% Silica calculated on the basis of millbase (solids): 11.7% Silica calculated on the basis of lacquer (total): 5.0% Silica calculated on the basis of lacquer (solids): 8.0%

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Production and application of the lacquers

The binder is mixed with the solvents. Then, for the purpose of predispersion, the silica is incorporated into this mixture with the high-speed mixer (disk \emptyset 45 mm) and predispersed for 5 min at 2000 rpm. The mixture is dispersed in a laboratory pearl mill for 30 min at 2500 rpm and 60% pump capacity using glass beads (\emptyset approx. 1 mm). The millbase is tested with a grindometer, 25 μ m, in accordance with DIN ISO 1524. It must be smaller than 10 μ m.

The conversion of the millbase to lacquer takes place in accordance with the formulation, the components being mixed with a vane agitator at 2000 rpm. The hardener is incorporated in the same way.

After adjusting the lacquers to spray viscosity in accordance with DIN 53411, the lacquers are applied to black lacquered metal sheets, e.g. DT 36 (from Q-Panel), by spray application (coat thickness about 40-50 μm). After spraying, the metal sheets are dried for 24 h at room temperature and then for 2 h in a drying oven at 70°C.

Scratch tests:

The metal sheets are abraded with a quartz/water slurry (100 g water + 1 g Marlon A 350, 0.25% + 5 g Sikron F500) using an abrasion and washing resistance tester (Erichsen, brush with hog's bristles). The gloss before and 10 min after the abrading is determined with a reflectometer (20° irradiation angle).

<u>Table 8:</u> Summary of the properties of the liquid lacquers relevant in terms of lacquer technology, and of the applied and dried films.

	Comparative silica 1	Silica 7	Silica 8	Reference without silica
Bulk density [g/l]	50	146	123	/
Grindometer value $[\mu m]$	< 10	< 10	< 10	/
Viscosity (millbase) [mPas]				
6 rpm	767 717	376 359	376 361	205 205
Viscosity (lacquer + hardener) [mPas] 6 rpm		279	281	120
60 rp m	399	272	274	120
Flow	poor (fine "cracks")	OK	OK	OK
Scratch resistance				
20° reflectometer value before scratching	82.3	86.5	86.3	88.2
Haze before scratching	3	4	4	2
Black value My	275	283	282	292
40 strokes with Sikron F 500 residual gloss [%]	63.2	78.2	75.4	30.2

⁵ The silicas 7 + 8 according to the invention can be used in high concentrations without impairing the appearance of the lacquer surface owing to their substantially lower rheological efficiency compared with comparative silica 1. In addition, the silicas according to the invention display a substantial improvement in the scratch resistance of the lacquer surface.

Example 3:

For the investigation of the improvement of the scratch resistance, a conventional 2-component polyurethane lacquer was used. The formulation of the lacquer and its production, including its application, are summarised below:

Formulation

Millbase	Parts by wt.
Acrylic copolymer, mod. with synthetic fatty acids, 60% solution	43.4
Butyl acetate 98%	17.8
Xylene	3.9
Silica	5.0
Σ	70.7
Lacquer make-up	
Xylene	11.3
Ethoxypropyl acetate	3.4
Butyl glycol acetate	1.6
Aliphatic polyisocyanate, approx. 75% in 1-methoxypropyl-2-	
acetate/xylene 1:1	18.6
Σ	105.0

Binder concentration:

Silica calculated on the basis of millbase (solids): 19.2%

Silica calculated on the basis of lacquer (total): 5.0%

Silica calculated on the basis of lacquer (solids): 12.5%

Production and application of the lacquers

15 The binder is mixed with the solvents. Then, for the purpose of predispersion, the silica is incorporated into this mixture with the high-speed mixer (disk \emptyset 45 mm) and predispersed for 5 min at 2000 rpm. The mixture is

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dispersed in a laboratory pearl mill for 30 min at 2500 rpm and 60% pump capacity using glass beads (\varnothing approx. 1 mm). The millbase is tested with a grindometer, 25 μ m, in accordance with DIN ISO 1524. It must be smaller than 10 μ m.

The conversion of the millbase to lacquer takes place in accordance with the formulation, the components being mixed with a vane agitator at 2000 rpm. The hardener is incorporated in the same way.

10 After adjusting the lacquers to spray viscosity in accordance with DIN 53411, the lacquers are applied to black lacquered metal sheets, e.g. DT 36 (from Q-Panel), by spray application (coat thickness about $40-50~\mu\text{m}$). After spraying, the metal sheets are dried for 24 h at room temperature and then for 2 h in a drying oven at 70°C .

Scratch tests:

The metal sheets are abraded with a quartz/water slurry (100 g water + 1 g Marlon A 350, 0.25% + 5 g Sikron F500) using an abrasion and washing resistance tester (Erichsen, brush with hog's bristles). The gloss before and 10 min after the abrading is determined with a reflectometer (20° irradiation angle).

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Table 9: Summary of the properties of the liquid lacquers relevant in terms of lacquer technology, and of the applied and dried films.

	Comparative silica 1	Silica 7 Silica	Silica 8	Reference without silica	Comparative silica 2	Silica 9	Silica 11	Reference without silica
Grindometer value [µm]	< 10	< 10	< 10	/	< 10	< 10	< 10	/
Viscosity (millbase) [mPas]								
6 rpm 60 rpm	409 407	210 210	220 212	, ,	5670 1260	935 409	832 407	. /
Viscosity (lacquer + hardener) [mPas]								
mdx 99 mdx 09	120 113	82	80	60	194	195 146	175 144	55 64
Flow	Poor fine cracks	OK	OK	ОК	Orange-peel effect	ОК	ОК	ОК
Scratch resistance			:					
20° reflectometer value before scratching	81	89.5	89.1	91.3	38	85.5	85.3	91.7
Haze before scratching	101	6	13	2	423	18	19	2
40 strokes with Sikron F 500 Residual gloss [%]	83.4	5.88	90.7	51.8	,	80.4	84.3	56.1

The silicas 7 + 8 and 9 + 10 according to the invention can be used in high concentrations without impairing the appearance of the lacquer surface owing to their substantially lower rheological efficiency compared with comparative silica 1 and 2. In addition, the silicas according to the invention display a substantial improvement in the scratch resistance of the <u>lacquer</u> surface.

Example 4

Direct comparison of the silicas according to the invention with a scratch-resistant lacquer according to DE 198 11 790 A1, in which AEROSIL R 972 is used to improve the scratch resistance.

		Prior art 1)	Silicas 2) according to the invention
	Millbase		
	Desmophen A 2009/1		190.2
	Methoxypropyl acetate: Solvesso 100 1:1		36.8
	Silica		23.0
15 ·	Σ		250.0
	Lacquer make-up		
	Desmophen A YEP4-55A, contains AEROSIL R 972	96.0	-
	Millbase	-	48.9
	Desmophen 2009/1	-	24.9
	OL 17, 10% in MPA	-	_
	Modaflow 1% in MPA	-	
	MPA : Solvesso 100 1:1	11.6	33.8
	Butyl glycol acetate	10.5	10.5
	Byketol OK	7.5	7.5
	Byk 141	0.8	0.8
	Addition of hardener		
	Desmodur N 3390	23.6	23.6
	Σ	150.0	150.0

5

Production and application of the lacquers

- 1) Comparative silica 1 is incorporated into the binder in accordance with DE 198 11 790 A1 using a jet disperser.
- The binder is mixed with the solvents. Then, for the purpose of predispersion, the silica is incorporated into this mixture with the high-speed mixer (disk Ø 45 mm) and predispersed for 5 min at 2000 rpm. The mixture is dispersed in a laboratory pearl mill for 30 min at 2500 rpm and 60% pump capacity using glass beads (Ø approx. 1 mm). The millbase is tested with a grindometer, 25 μm, according to DIN ISO 1524. It must be smaller than 10 μm.
- 15 The conversion to lacquer of the millbases corresponding to 1) or 2) takes place in accordance with the formulation, the components being mixed at 2000 rpm with a vane agitator. The hardener is incorporated in the same way.
- After adjusting the lacquers to spray viscosity in accordance with DIN 53411, the lacquers are applied to black lacquered metal sheets, e.g. DT 36 (from Q-Panel), by spray application (coat thickness about 40-50 μm). After spraying, the metal sheets are dried for 24 h at room temperature and then for 2 h in a drying oven at 70°C.

25 <u>Scratch tests:</u>

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The metal sheets are abraded with a CaCO₃/water slurry (100 g water + 1 g Marlon A 350, 0.25% + 5 g Millicarb CaCO₃) using an abrasion and washing resistance tester (Erichsen, brush with hog's bristles). The gloss before and 10 min after the abrading is determined with a reflectometer (20° irradiation angle).

Table 10: Summary of the properties of the liquid lacquers relevant in terms of lacquer technology, and of the applied and dried films.

	Prior art	Silica 7	Reference
Grindometer value [μm]	< 10	< 10	/
Viscosity (millbase) [mPas]			
6 rpm 60 rpm	58 48	30 43	30 40
Surface	Orange peel	OK	OK
20° reflectometer value before scratching	88.0	86.5	98.5
100 strokes with Millicarb Residual gloss [%]	88.6	96.3	59.6

5

It is shown that a substantially better improvement in the residual gloss is achieved after a scratch stressing of the lacquer surface by using the silica according to the invention than with the prior art. In addition, owing to its low rheological efficiency, the silica according to the invention does not cause an orange-peel effect.

Claims:

- Silanised, structurally modified, pyrogenically produced silicas, characterised by groups fixed to the surface, wherein
- the groups are alkylsilyl (SiC_nH_{2n+1} , with n=2-18).
- 2. Silanised, structurally modified, pyrogenically produced silicas according to claim 1, characterised in that the pyrogenically produced silicas have been treated with the compound (CH₃O)₃SiC₁₆H₃₃ (hexadecyltrimethoxysilane).
 - 3. Silanised, structurally modified, pyrogenically produced silicas according to claim 1, characterised in that
- the pyrogenically produced silicas have been treated with the compound $(CH_3O)_3SiC_8H_{17}$ (octyltrimethoxysilane).
 - 4. Process for the production of the silanised, structurally modified, pyrogenically produced silicas according to claims 1 to 3,
- characterised in that the pyrogenically produced silicas are placed in a mixer, the silicas are sprayed, optionally first with water and then with the compound from the group (RO)₃SiC_nH_{2n+1} while mixing intensively, mixed for a
- further 15 to 30 minutes and then tempered at a temperature of 100 to 160°C for a period of 1 to 3 hours, structurally modified and/or optionally postground.
- 5. Process for the production of the silanised,
 structurally modified, pyrogenically produced silicas according to claim 4,
 characterised in that

an additional tempering is allowed to follow the stuctural modification and/or post-grinding.

6. Use of the silanised, structurally modified,
 pyrogenically produced silicas to improve the scratch
 resistance of lacquers.

INTERN IONAL SEARCH REPORT

International Pilication No PCT/ 3/08329

A. CLASSIFICATION OF SUBJECT MATTER IPC 7 C09C1/30 C09D7/12

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols) IPC 7 C09C C09D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, PAJ, WPI Data, CHEM ABS Data

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the whole document	4,5
US 5 776 240 A (MEYER JUERGEN ET AL) 7 July 1998 (1998-07-07)	1
column 2, line 15 -column 3, line 29 column 5, line 32 - line 33 column 10, line 20 - line 34 tables	4,5
US 5 959 005 A (HENNIG THOMAS ET AL) 28 September 1999 (1999-09-28) the whole document	4
	20 September 1995 (1995-09-20) cited in the application the whole document US 5 776 240 A (MEYER JUERGEN ET AL) 7 July 1998 (1998-07-07) column 2, line 15 -column 3, line 29 column 5, line 32 - line 33 column 10, line 20 - line 34 tables US 5 959 005 A (HENNIG THOMAS ET AL) 28 September 1999 (1999-09-28)

χ Further documents are listed in the continuation of box C.	χ Patent family members are listed in annex.
 Special categories of cited documents: 'A' document defining the general state of the art which is not considered to be of particular relevance 'E' earlier document but published on or after the international filling date 'L' document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) 'O' document referring to an oral disclosure, use, exhibition or other means 'P' document published prior to the international filling date but later than the priority date claimed 	 "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art. "&" document member of the same patent family
Date of the actual completion of the international search 30 October 2003	Date of mailing of the international search report $06/11/2003$
Name and malling address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL – 2280 HV Rijswijk Tel. (+31–70) 340–2040, Tx. 31 651 epo nl, Fax: (+31–70) 340–3016	Authorized officer Nobis, B

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International lication No
PCT/ 3/08329

		PCT/ 3/08329
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